A vectorial solver for the reflection of semi-confined waves at slab waveguide discontinuities for non-perpendicular incidence

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4 Rectangular slab waveguide facet

1 Oblique incidence at a slab discontinuity

The effects of transitions between regions with different layering on thin-film guided, in-plane unguided light form the basis for a series of classical integrated optical components [1, 2]. Concepts have been discussed for lenses [3, 4], mirrors [5], prisms [6], but also for complex lens-systems [7], or, more recently, for entire spectrometer [8]. The relevant interfaces are either straight, or merely slightly curved, permitting (b) The retevant metrates are enter straight, of metry straight curved, permuting a description of the in-plane wave propagation in terms of geometrical optics. Hence we take a closer look at what happens to vertically guided, laterally plane waves at straight interfaces, facets, or transition regions with other cross section shapes.



While standard scalar TE / TM Helmholtz equations apply for perpendicular incidence, for non-normal incidence one is led to a vectorial problem [9] that is formally identi-cal to that for the modes of 3-D channel waveguides. Here, however, it needs to be cal to that for the modes of 3-D channel waveguides. Here, however, it needs to be solved as a parametrized, inhomogeneous system on a 2-D computational window with transparent-influx boundary conditions. As a step beyond the scalar approximation [9], and older bidirectional approaches [10, 11], we here report on a dedicated vectorial solver for — in principle — arbitrary rectangular cross section geometries, based on simultaneous expansions into slab modes along *two* orthogonal coordinate axes [12].

2 Vectorial quadridirectional eigenmode propagation

· Homogeneous Maxwell equations, frequency domain, linear dielectric media, $\operatorname{curl} \bar{\boldsymbol{E}} = -\mathrm{i}\omega\mu_0\bar{\boldsymbol{H}}, \quad \operatorname{curl} \bar{\boldsymbol{H}} = \mathrm{i}\omega\epsilon\epsilon_0\bar{\boldsymbol{E}}$ for electric and magnetic fields $\tilde{E},\tilde{H},$ oscillating $\sim \exp(i\omega t)$ in time with frequency $\omega=kc=2\pi c/\lambda,$ for vacuum wavenumber k, wavelength $\lambda,$ speed of light c, permittivity ϵ_0 , and permeability μ_0 .



- Incoming field: slab mode with $\beta_{in} = kN_{in}$ at angle $\theta \longrightarrow k_y(\theta) = kN_{in}\sin\theta$ • Mode types (z-propagating / -evanescent) change with θ : $k_z(\theta) = \pm \sqrt{\beta^2 - k_y^2(\theta)}$.
- Expand the electromagnetic field into local sets of TE & TM eigenme
- Bidirectional mode overlaps along all interfaces



Vectorial quadridirectional eigenmode propagation (vOUEP)

3 Critical angles

Uniform $k_y = k N_{\rm in} \sin \theta$ related to incoming mode $(N_{\rm in})$ & incidence angle Outgoing modes ($N_{\rm out}$) leave at angles $\theta_{\rm out}$ with $k_y = kN_{out} \sin \theta_{out}$, different for every outgoing mode; generalized Snell's law: $N_{out} \sin \theta_{out} = N_{in} \sin \theta$,

applicable to all (reflected, transmitted, up- or downwards scattered) outgoing propagating modes

- Outgoing modes with $N_{\rm out} \leq N_{\rm crit}$ become evanescent for incidence angles $\theta \geq \theta_{\rm crit}$ with $\sin \theta_{\rm crit} = N_{\rm crit}/N_{\rm in}$, i.e. these modes do not carry power away Relevant values for the following examples:
- sin θ_c = n_c/N_{in}, no forward/backward power loss into the cover for θ ≥ θ_c.
 sin θ_s = n_s/N_{in}, no forward/backward power loss into the substrate for θ ≥ θ_s. • in: TE₀, $\sin \theta_{\rm m} = N_{\rm TM0}/N_{\rm TE0}$, no power conversion to refl. TM₀ mode for $\theta \ge \theta_{\rm m}$



0 z [μm]

Beam displacement









7 Strip waveguide, lateral excitation

ergy density) dx dz, θ_{TF00} , θ_{TM00} : strip, vectorial modes (WMM [13])





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9 References

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